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Revision: R1

DESIGN REVIEW REPORT
FOR
SKY BRIDGE
AT
DESSERT ROCK HOTEL_SAUDI
ARABIA
FOR
WARRIOR GROUP



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Submitted By



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Table of Contents

1.	INTRODUCTION	3
2.	GEOMETRY	4
3.	PROPERTY.....	6
4.	LOADING	7
5.	LOAD CASES.....	7
6.	LOAD COMBINATIONS	8
7.	ANALYSIS & DESIGN RESULTS	9
7.1.	SUMMARY OF SAP 2000 RESULTS WITH BRIDGE DESIGN STANDARD OF NEPAL.....	9
7.2.	ANALYSIS OF CABLES USING LSTB STANDARD TECHNICAL MANUAL VOLUME A	10
7.3.	ANALYSIS & DESIGN RESULTS OF DECK STRUCTURE	12
7.3.1.	3D model of Deck Structure for Sky Bridge	12
7.3.2.	Deformed shape of Deck Structure	12
7.3.3.	Stress Diagram of the cross beam for SVM.....	13
8.	CHECK FOR CONNECTION DESIGN.....	14
8.1.	CABLE – ANCHOR CONNECTION.....	14
8.1.1.	Adjustable Pin Connection	15
8.1.2.	Hinged Pin Connection	17
8.1.3.	Bracket Connection	19
8.1.4.	Base-plate Connection	21
8.2.	GROUND ANCHOR CONNECTION.....	23
9.	CONCLUSION	24



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1. INTRODUCTION

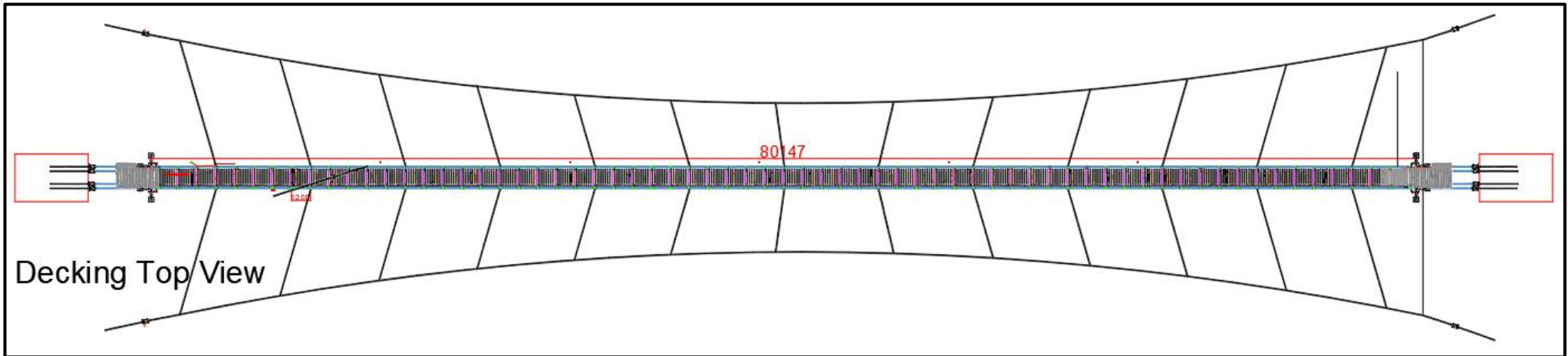
This design review report presents design review for SKY BRIDGE structure for proposed Dessert rock hotel at Saudi Arabia. It includes codes referred for analysis & loading considerations, SAP 2000 modeling, analysis & design results and connection design. Refer below images showing layout and structural systems of proposed SKY BRIDGE structure.

Following documents were referred in review of Sky Bridge structure:

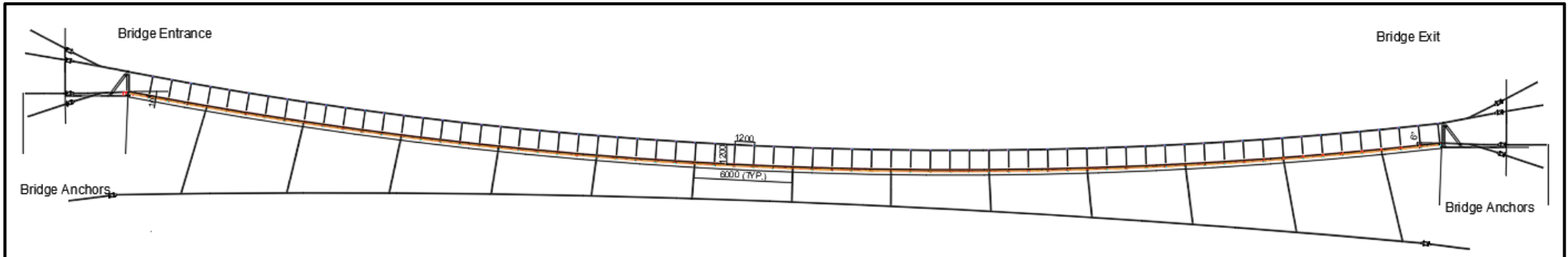
1. Architectural Drawing: Sky Bridge Structure
(Drawing number R01-H13C13-WES-2R-ZZ-DWG-AR-00001/10001/20001/30001/50001/90001)
2. Structural drawing: Sky Bridge Structure
(Drawing number R01-H13C13-WES-2R-ZZ-DWG-ST-10001/20001/20002/30001/50001/50002/50003/90001/90002)
3. SAP 2000 model
(Model name: dubai new sb cable final final with sag 4.45 m from left support copy 4444 with wg 66666.sdb,
Model name: dubai new 15 degree down HC in lower side.sdb)
4. Design Summary & Compliance Report (Ref no. WE-RSG-SKYB-DSCR, Rev: 1.0)
5. Design Summary Report of SAP Analysis of Deck Structure (Ref no. RN-WG-SKYB-DSDS, Rev: 0.0)
6. Design Summary & Compliance Report (Ref no. RN-WG-SKYB-DCCON, Rev: 0.0)
7. Ground Anchor Design Philosophy Report (Ref no. 1799/TN01)
8. Design Calculations of End Connection of Cross Beam (Ref no. RN-WG-SKYB-DCECCB, Rev: 0.0)



2. GEOMETRY



SKY BRIDGE layout (Plan View)

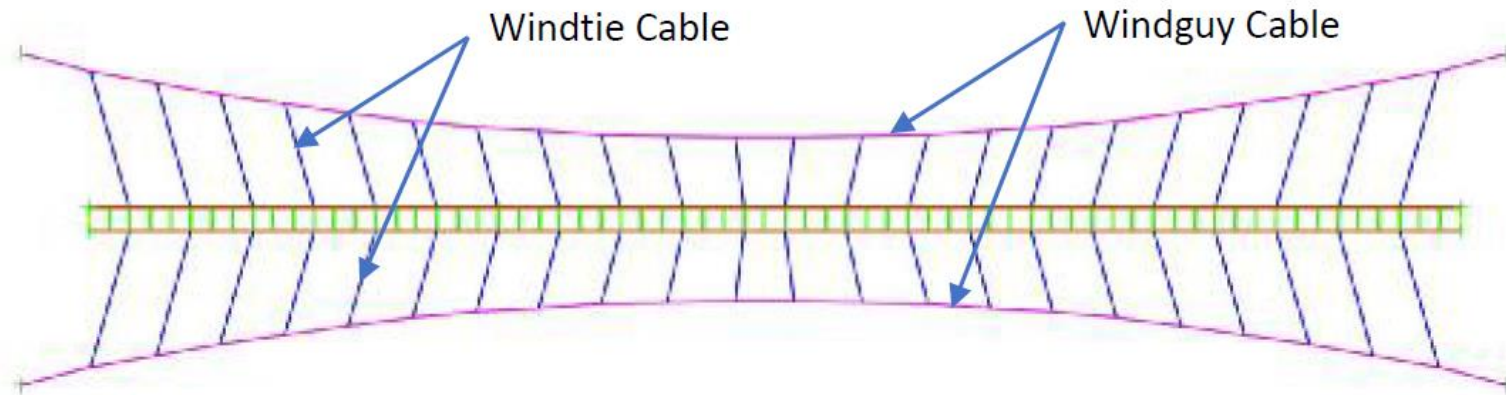


SKY BRIDGE Elevation (Side View)

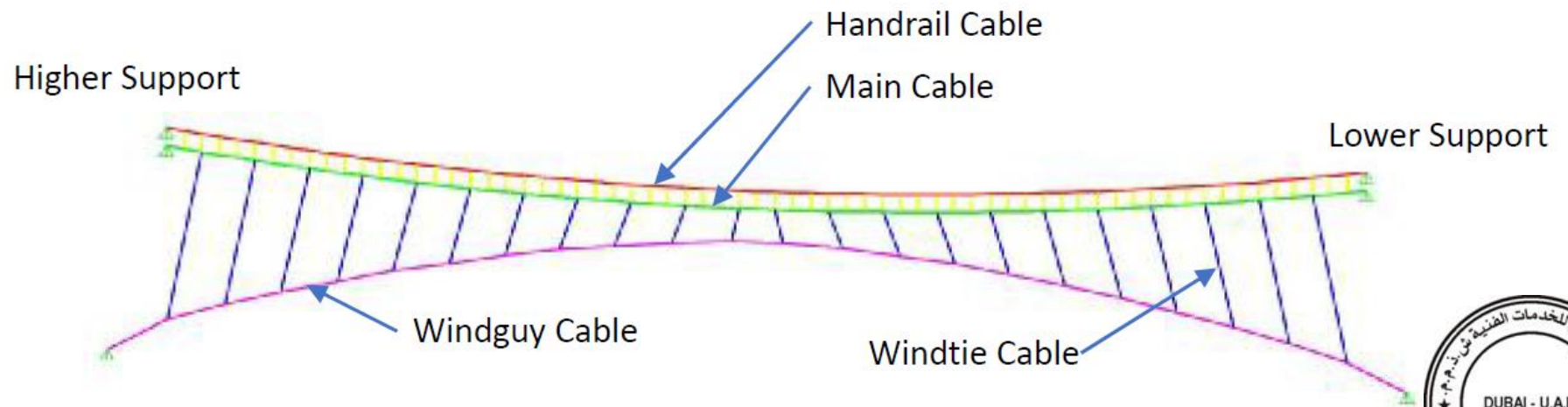
- SAP 2000 model geometry



Dehman



PLAN



ELEVATION



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3. PROPERTY

Assigned member property of SKY BRIDGE in SAP 2000 model.

TABLE: Frame Section Properties 01 - General

SectionName	Material	Shape	t3	t2	tf	tw	FilletRadius	Area	TotalWt	TotalMass
Text	Text	Text	m	m	m	m	m	m2	KN	KN-s2/m
Cross Beam ISMC100	Fe250	Channel	0.1	0.05	0.0075	0.0047	0	0.00117	7.961	0.81
Hand Rail Cable 1x48mm	Fe250	Circle	0.04					0.001257	15.536	1.58
Main Cable 2x48mm	Fe250	Circle	0.056					0.002463	30.45	3.1
Suspender 16mm	Fe250	Circle	0.016					0.000201	2.451	0.25
Wind Guy 40mm	Fe250	Circle	0.033					0.000855	11.81	1.2
Wind Tie	Fe250	Circle	0.011					0.000095	2.604	0.27

TABLE: Area Section Properties

Section	Material	MatAngle	AreaType	Type	Thickness
Text	Text	Degrees	Text	Text	m
deck	Fe250	0	Shell	Membrane	0.007

SKY BRIDGE – Property



4. LOADING

Summary of loadings in SAP2000

Loads		Values	Unit	Remarks
Live Load		5.20	kN/m	In vertical down direction
Dead Load				
	Self-weight of overall bridge components excluding utility load	Equivalent section/frame sizes.		
	Utility Load	0.60	kN/m	Loaded along the main cable in vertical down direction
	Wind Load	0.50	kN/m	Loaded along the one wind guy cable in horizontal direction

5. LOAD CASES

TABLE: Load Case Definitions

Case	Type	DesignType	RunCase
Dead	LinStatic	Dead	Yes
MODAL	LinModal	Other	Yes
utility load	LinStatic	Dead	Yes
Live	LinStatic	Live	Yes
Winy	LinStatic	Wind	Yes



6. LOAD COMBINATIONS

As per the AISC-LRFD93, following load combinations are considered for the SAP2000 analysis.

TABLE: Combination Definitions						
ComboName	ComboType	CaseType	CaseName	ScaleFactor	SteelDesign	Notes
COMB1	Linear Add	Linear Static	Dead	1	None	
COMB1		Linear Static	utility load	1		
COMB1		Linear Static	Live	1		
UDSTL1	Linear Add	Linear Static	Dead	1.4	Strength	Dead Only; Strength
UDSTL1		Linear Static	utility load	1.4		
UDSTL2	Linear Add	Linear Static	Dead	1.2	Strength	Dead + Live; Strength
UDSTL2		Linear Static	utility load	1.2		
UDSTL2		Linear Static	Live	1.6		
UDSTL3	Linear Add	Linear Static	Dead	1.2	Strength	
UDSTL3		Linear Static	utility load	1.2		
UDSTL3		Linear Static	Live	0.5		
UDSTL3		Linear Static	Winy	1.3		
UDSTL4	Linear Add	Linear Static	Dead	1.2	Strength	
UDSTL4		Linear Static	utility load	1.2		
UDSTL4		Linear Static	Live	0.5		
UDSTL4		Linear Static	Winy	-1.3		
UDSTL5	Linear Add	Linear Static	Dead	1.2	Strength	Dead + Wind; Strength
UDSTL5		Linear Static	utility load	1.2		
UDSTL5		Linear Static	Winy	1.3		
UDSTL6	Linear Add	Linear Static	Dead	1.2	Strength	Dead - Wind; Strength
UDSTL6		Linear Static	utility load	1.2		
UDSTL6		Linear Static	Winy	-1.3		
UDSTL7	Linear Add	Linear Static	Dead	0.9	Strength	Dead (min) + Wind; Strength
UDSTL7		Linear Static	utility load	0.9		
UDSTL7		Linear Static	Winy	1.3		
UDSTL8	Linear Add	Linear Static	Dead	0.9	Strength	Dead (min) - Wind; Strength
UDSTL8		Linear Static	utility load	0.9		
UDSTL8		Linear Static	Winy	-1.3		
UDSTL9	Linear Add	Linear Static	Dead	1	Deflection	Dead Only; Deflection
UDSTL9		Linear Static	utility load	1		
UDSTL10	Linear Add	Linear Static	Dead	1	Deflection	Dead + Live; Deflection
UDSTL10		Linear Static	utility load	1		
UDSTL10		Linear Static	Live	1		



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7. ANALYSIS & DESIGN RESULTS

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7.1. Summary of SAP 2000 results with bridge design standard of Nepal

1. BASIC INFORMATION			
Span	L	80.00 m	
Difference in Elevation between saddles	h	3.00 m	
2. CABLE CONFIGURATION			
No of Main Cable		4	
Dia of Main Cable		48 mm	
No of Handrail Cable		2	
Dia of Handrail Cable		48 mm	
No of Windguy Cable		2	
Dia of Windguy Cable		40 mm	
3. LOADS			
Hoisting Load (Main Cable)	gh	0.565 kN/m	
Total Dead Load	gd	1.578 kN/m	
Load from Utility Pipe		0.600 kN/m	
Live Load		5.20 kN/m	
Total Full Load	gf	7.378 kN/m	
4. SAG CONSIDERED FOR MAIN CABLES			
Dead Load Sag	bd	2.75 m	
Full Load Sag	bf	3.469 m	
5. CABLE INCLINATION (HIGHER SUPPORT)			
Dead Load	bd	9.93 Degrees	
Full Load	bf	11.913 Degrees	
Standard Requires angle of inclination to be less than 12 Degree in Dead Load Case			OK
6. CABLE TENSION			
6.1 Cable Tension from SAP Analysis (Unfactored)			
Tension on Main Cable for Two Cable	879.48	kN	
Tension on Handrail Cable for Single Cable	157.44	kN	
Minimum Braking Load for Two 48 mm Cable	3228	kN	Wire Strength of 1960 N/mm2
Factor of safety of Main Cable	3.67	>	
Standard requires a safety margin of >3			
Result			OK
Minimum Braking Load for Single 48 mm Cable	1614	kN	Wire Strength of 1960 N/mm2
Factor of safety of Handrail Cable	10.25		
Result			OK

Design



7.2. Analysis of Cables using LSTB Standard Technical Manual Volume A

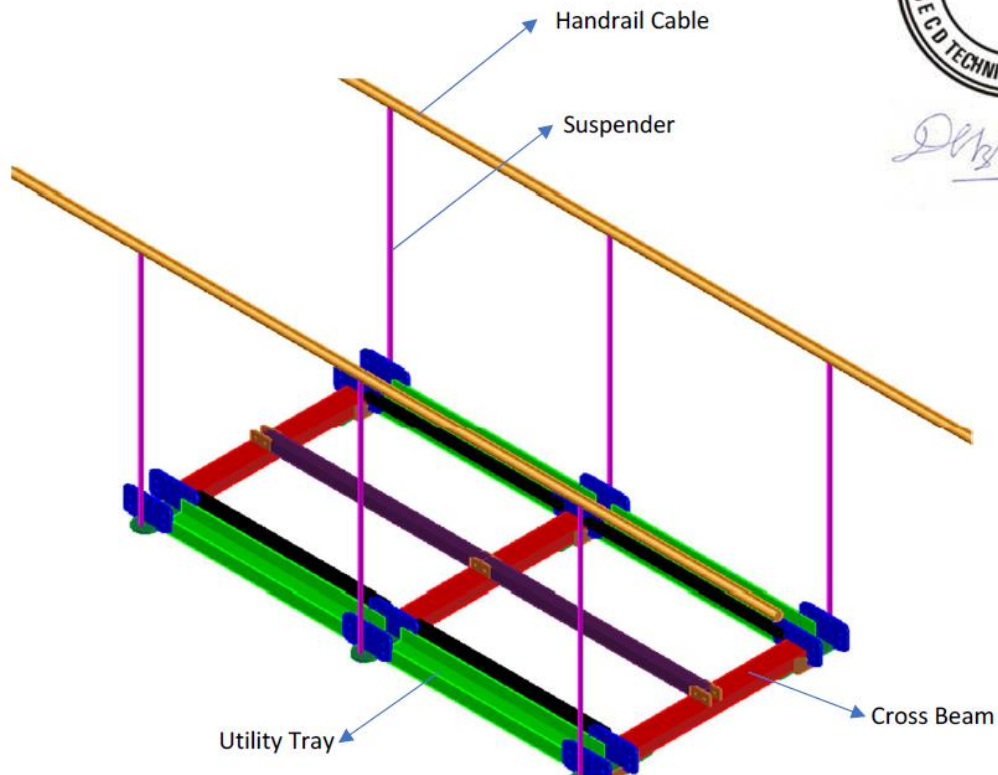
BASIC INFORMATION			
Span	L	80.00	m
Difference in Elevation between saddles	h	3.00	m
CABLE CONFIGURATION			
No of Main Cable		4	
Dia of Main Cable		48	mm
No of Handrail Cable		2	
Dia of Handrail Cable		48	mm
No of Windguy Cable		2	
Dia of Windguy Cable		40	mm
Modulus of Elasticity of Steel Wire Rope			
E		110	kN/m ²
Design Load Calculations			
1. Hoisting Load Case			
Main Cable and Handrail Cable	gh	0.565	kN/m
2. Dead Load Case			
Hoisting Load (main cable)		0.565	kN/m
Deck including Longitudinal Beam, Cross Beam and utility supports		0.720	kN/m
Windguy Cable with Windtie		0.292	kN/m
Total Dead Load	gd	1.578	kN/m
3. Load from Utility Pipe			
		0.600	kN/m
4. Full Load Case			
Dead Load		1.578	kN/m
Live Load		5.20	kN/m
Utility Load		0.60	kN/m
Total Full Load	gf	7.378	kN/m
Sag Calculation			
Dead Load Sag	bd	2.75	m
Length of Cable at Dead Load Case	Ld	80.308	m
Constant Factor,	C	0.3470	
Hoisting Load Sag (By Iteration)			
b*		2.558	m
g*		0.565	kN/m
new b*		2.558	m

Difference between b^* and new b^*			0.000	
Hoisting Load Sag b_h			2.558	m
Full Load Sag (By Iteration)				
b^*			3.469	m
g^*			7.378	kN/m
new b^*			3.469	m
Difference between b^* and new b^*			0.000	
Full Load Sag b_f			3.469	m
Maximum Tension at Full Load	T_{max}		1738.58	kN
Factor of Safety for Cable Tension			4.41	
Calculation of Final Data				
Description	Unit	Hoisting Case	Dead Load Case	Full Load Case
Span, L	m	80		
Elevation Difference, h	m	3		
Metallic Area of Main Cable, A_m	mm ²	4053.41		
Metallic Area of Handrail Cable, A_h	mm ²	2026.70		
Total Metallic Area of Cable, A	mm ²	6080.11		
Load, g	kN/m	0.5652	1.578	7.378
Sag, b	m	2.558	2.75	3.469
Final Results				
Cable Inclination at Higher Side, β_1	Deg	9.39	9.93	11.91
Cable Inclination at Lower Side, β_2	Deg	5.17	5.71	7.74
Distance of lowest point of Parabola from Higher Side, e	m	51.726	50.909	48.647
Maximum Sag, f	m	4.278	4.250	4.969
Length of Cable, L	m	80.274	80.308	80.457
Horizontal Component of Cable Tension, H	kN	176.729	458.938	1701.137
Maximum Tension, T_{max}	kN	179.131	465.913	1738.584
Maximum Tension on Main Cable, T_{Mmax}	kN	119.421	310.608	1159.056
Tension on Main Cable, T_M	kN	118.300	307.485	1144.527
Maximum Tension on Handrail Cable, T_{Hmax}	kN	59.710	155.304	579.528
Tension on Handrail Cable, T_H	kN	59.150	153.742	572.264

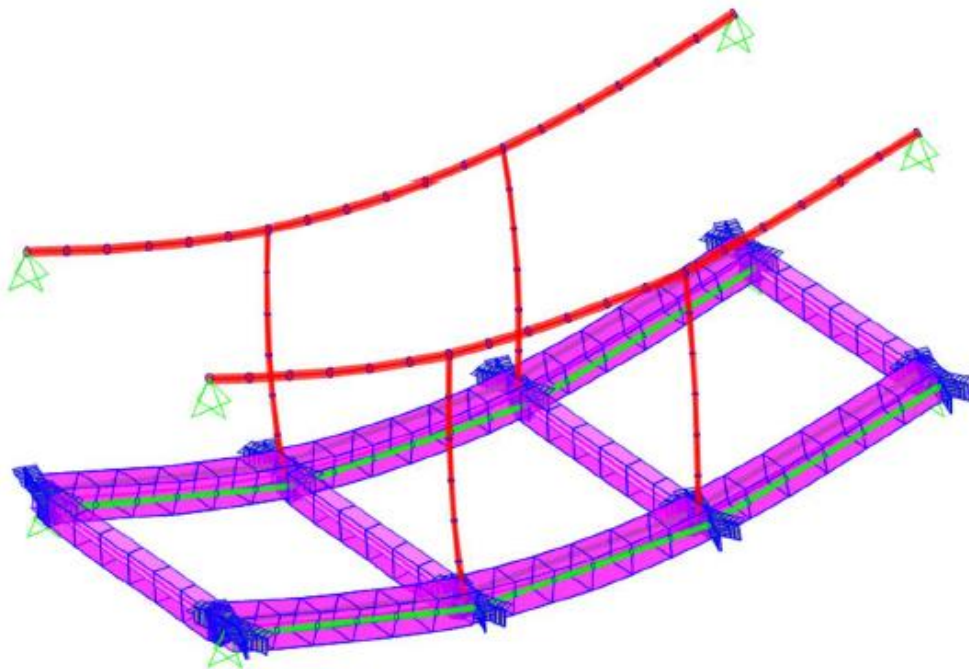


7.3. Analysis & Design results of Deck Structure

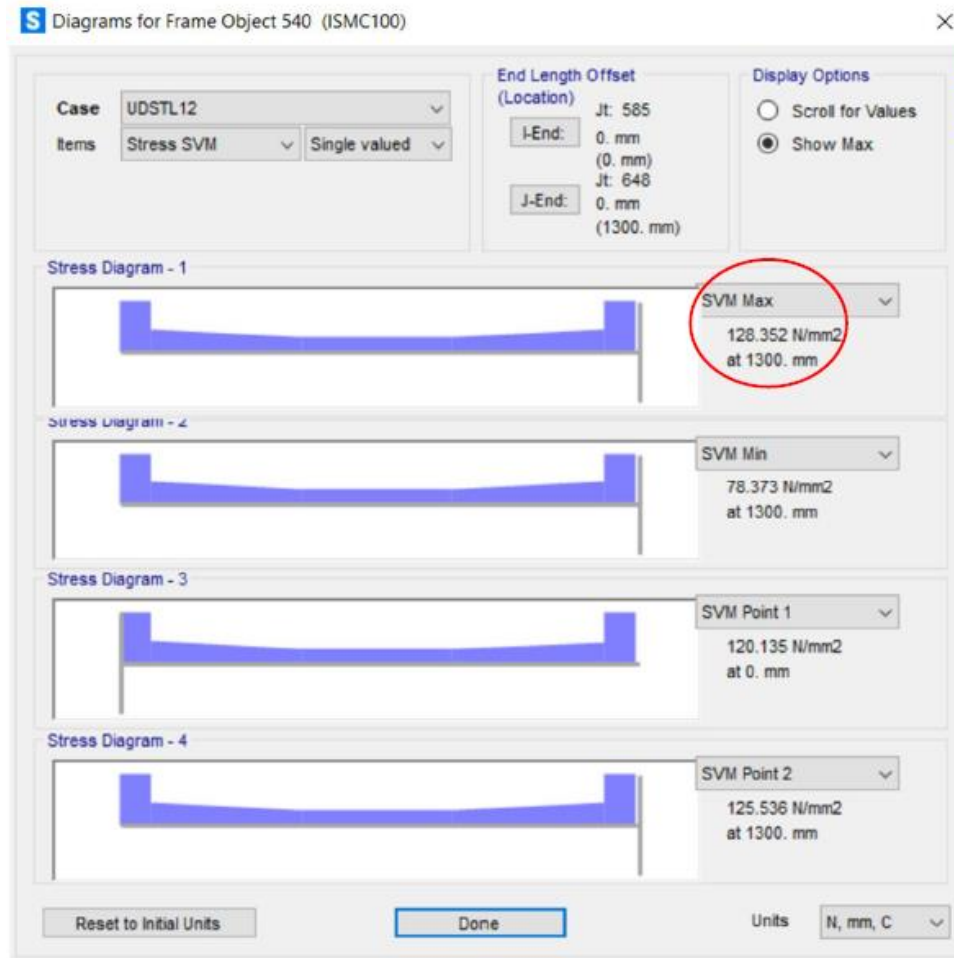
7.3.1. 3D model of Deck Structure for Sky Bridge



7.3.2. Deformed shape of Deck Structure



7.3.3. Stress Diagram of the cross beam for SVM



Actual von mis stress (SVM) = 128.352 MPa

Maximum allowable stress = 150 MPa

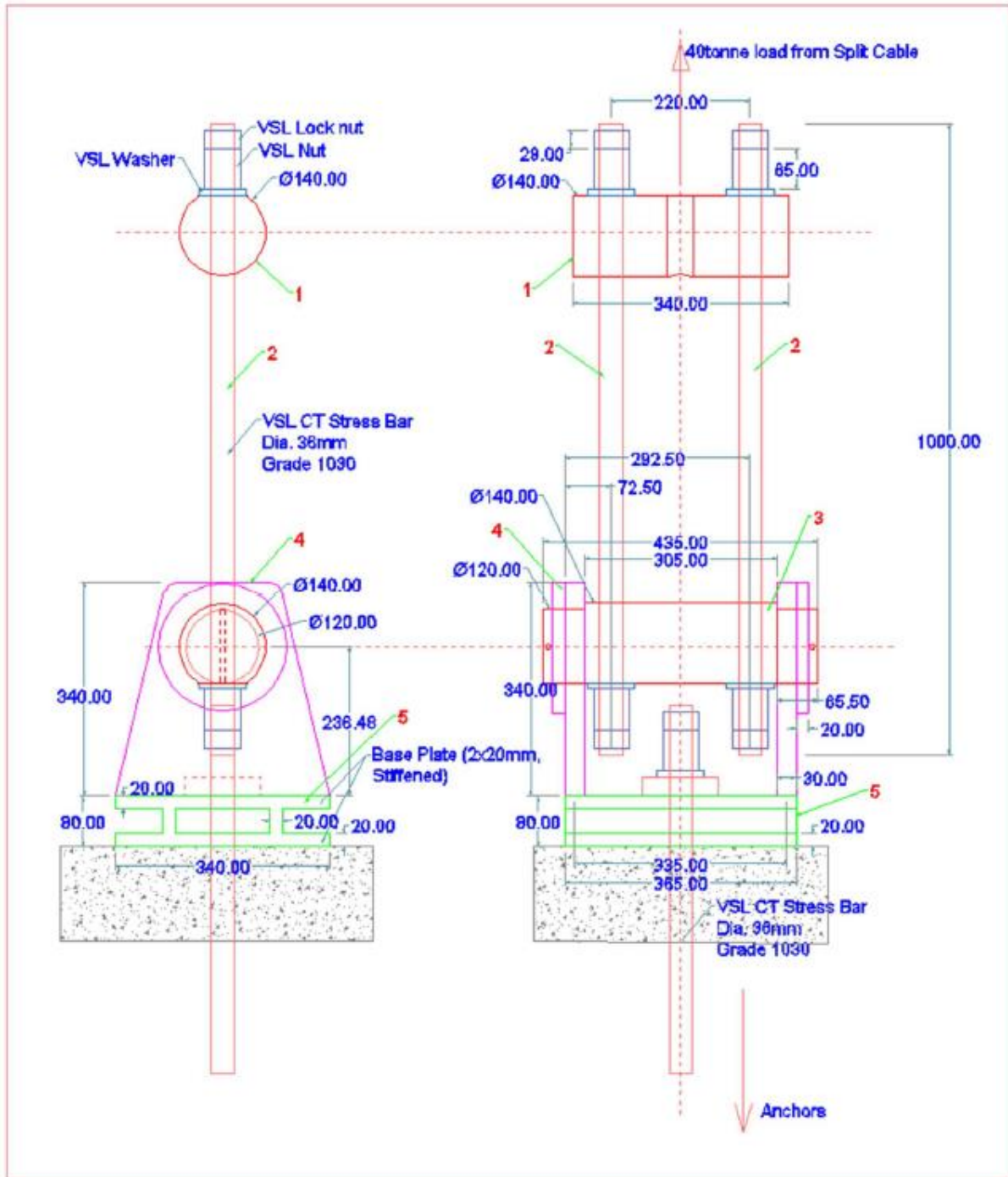
Actual stress of the cross beam < Maximum allowable stress (Hence OK)



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8. CHECK FOR CONNECTION DESIGN

8.1. Cable – Anchor Connection



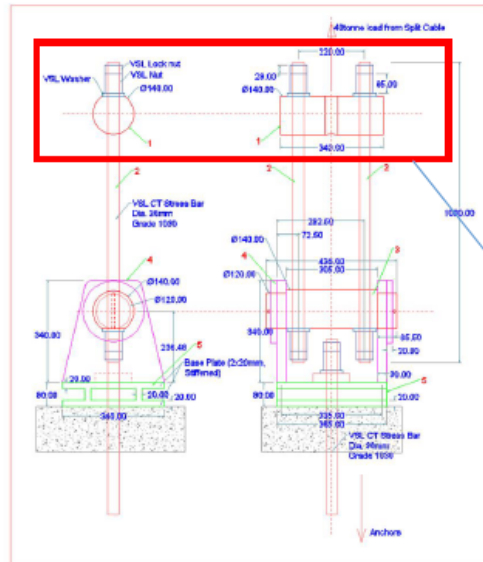
Cable-Anchor Connection

Part List

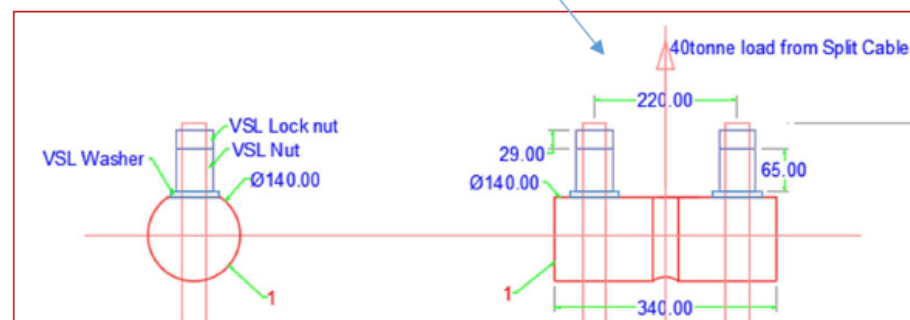
S.N.	Part Name	Material	Section	Dimensions (mm)	Qty.	Remarks
1	Adjustable Pin	Fe250	Round Bar	140 dia., L=340	1	
2	Thread Rod	VSL CT Stress Bar, Grade 1030	Thread rod	36 dia., L=1000	2	
3	Hinged Pin	Fe250	Round Bar	140 dia., L=340	1	
4	Brakcet	Fe250	Plate 30	340x340x30	2	
5	Base Plate	Fe250	2x stiffened Plate 20	2x (340x365x20)	1	

8.1.1. Adjustable Pin Connection

Cable-Anchor Connection						
Part List						
S.N.	Part Name	Material	Section	Dimensions (mm)	Qty.	Remarks
1	Adjustable Pin	Fe250	Round Bar	140 dia., L=340	1	
2	Thread Rod	VSL CT Stress Bar, Grade 1030	Thread rod	36 dia, L=1000	2	
3	Hinged Pin	Fe250	Round Bar	140 dia., L=340	1	
4	Brakcet	Fe250	Plate 30	340x340x30	2	
5	Base Plate	Fe250	2x stiffened Plate 20	2x (340x365x20)	1	

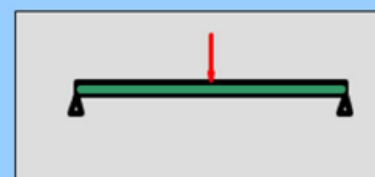


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- Check for Bending Stress:

Beam material			
List of materials	Structural steel EC 3, EN 10025; Fe 360 (210000)		
Density	γ	7850.0	[kg/m ³]
Modulus of elasticity in tension	E	210000	[MPa]
Permissible bending stress	σ_b	141	[MPa]
Results section			
✓ Calculation results			
Support number from left	R1	R2	
Reaction in supports	200114.61	200114.61	[N]
Bending moment Min. / Max.	M ₀	0.00	22006.30 [Nm]
Beam deflection Min. / Max.	y	-0.030	0.000 [mm]
Bending stress Min. / Max.	σ_b	0	102 [MPa]
Weight of the beam	m	22.9	[kg]
Max. length of the free end (buckling).	L _{max}	0.0	[mm]
Relative beam deflection Max.	γ'	0.014	[%]



- Check for Shear Stress:

Max. Shear Force : 20 ton

Shear Area : 10152 mm²

Now, the shear stress is calculated as

Permissible shear stress is

$$= \text{Yield Strength} \times 0.4$$

$$= 250 \text{ MPa} \times 0.4$$

$$= 100 \text{ MPa}$$

Max. Shear Stress = Max. Shear Force / Shear Area

$$= 20 \text{ ton} / 10152 \text{ mm}^2$$

$$= 19.70 \text{ MPa}$$

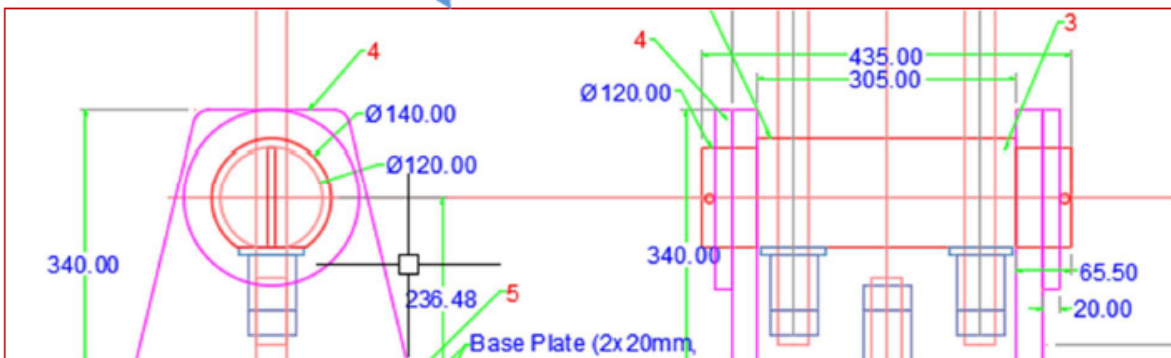
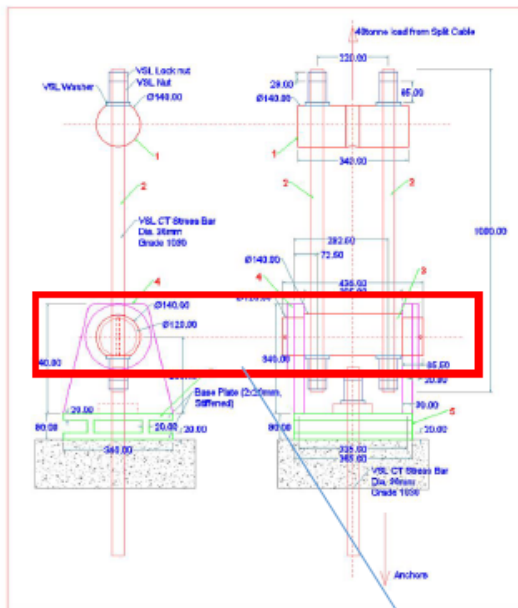
Which is less than the permissible shear stress, hence the selected size and material of this part is safe for shear strength.



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8.1.2. Hinged Pin Connection

Cable-Anchor Connection						
Part List						
S.N.	Part Name	Material	Section	Dimensions (mm)	Qty.	Remarks
1	Adjustable Pin	Fe250	Round Bar	140 dia., L=340	1	
2	Thread Rod	VSL CT Stress Bar, Grade 1030	Thread rod	36 dia, L=1000	2	
3	Hinged Pin	Fe250	Round Bar	140 dia., L=340	1	
4	Brakcet	Fe250	Plate 30	340x340x30	2	
5	Base Plate	Fe250	2x stiffened Plate 20	2x (340x365x20)	1	



- Check for Bending Stress:

✓ Beam type, dimensions and loading

Calculation units
SI Units (N, mm, kN/m...)

Left beam end
B...Support

Number of supports between
0

Right beam end
B...Support

Beam field no: **L1**

Length of beam field **L** 354.0 [mm]

Beam material

List of materials Structural steel EC 3, EN 10025; Fe 360 (210000)

Density γ 7850.0 [kg/m³]

Modulus of elasticity in tension E 210000 [MPa]

Permissible bending stress σ_b 141 [MPa]

Results section

✓ Calculation results

Support number from left	R1	R2			
Reaction in supports	199619.45	200749.40			[N]

Bending moment Min. / Max.	M_0	0.00	13471.92	[Nm]
Beam deflection Min. / Max.	y	-0.068	0.000	[mm]
Bending stress Min. / Max.	σ_b	0	62.5	[MPa]
Weight of the beam	m	36.9	[kg]	
Max. length of the free end (buckling).	L_{max}	0.0	[mm]	
Relative beam deflection Max.	y'	0.019	[%]	

- Check for Shear Stress:

Maximum shear force resulted as

Max. Shear Force : 20 ton

Shear Area : 10152 mm²

Now, the shear stress is calculated as

Permissible shear stress is

$$= \text{Yield Strength} \times 0.4$$

$$= 250 \text{ MPa} \times 0.4$$

$$= 100 \text{ MPa}$$

Max. Shear Stress = Max. Shear Force / Shear Area

$$= 20 \text{ ton} / 10152 \text{ mm}^2$$

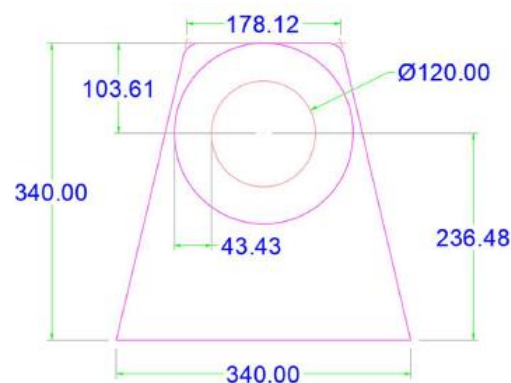
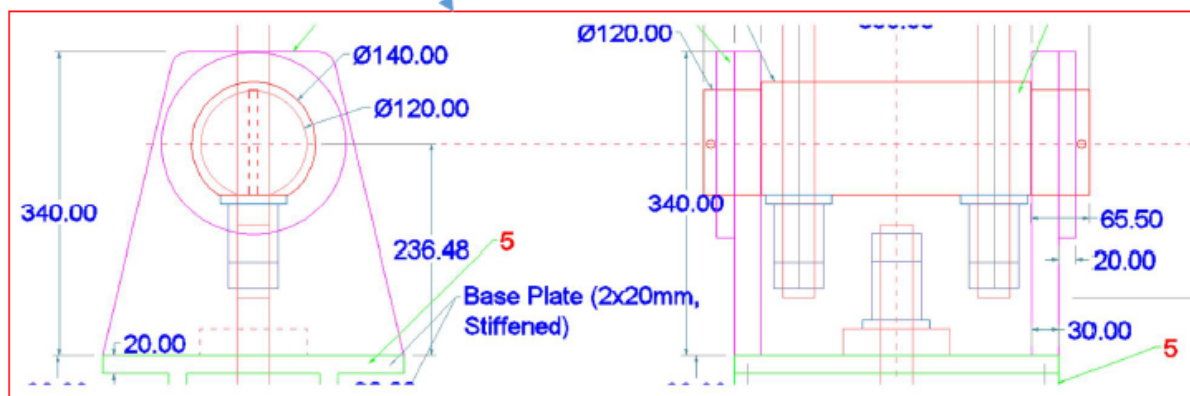
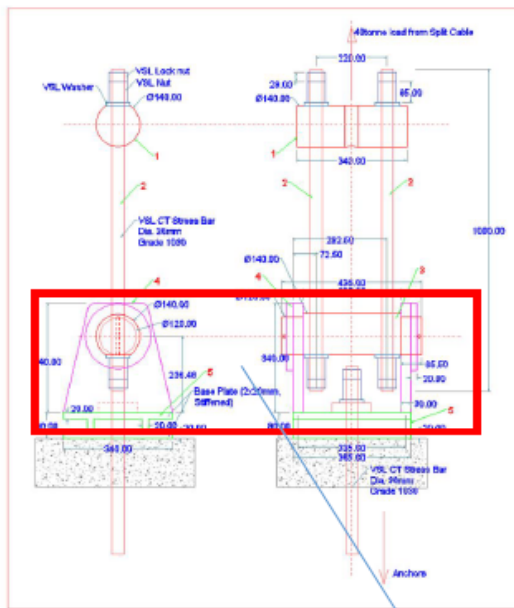
$$= 19.70 \text{ MPa}$$

Which is less than the permissible shear stress, hence the selected size and material of this part is safe for shear strength.



8.1.3. Bracket Connection

Cable-Anchor Connection						
Part List						
S.N.	Part Name	Material	Section	Dimensions (mm)	Qty.	Remarks
1	Adjustable Pin	Fe250	Round Bar	140 dia., L=340	1	
2	Thread Rod	VSL CT Stress Bar, Grade 1030	Thread rod	36 dia, L=1000	2	
3	Hinged Pin	Fe250	Round Bar	140 dia., L=340	1	
4	Brakcet	Fe250	Plate 30	340x340x30	2	
5	Base Plate	Fe250	2x stiffened Plate 20	2x (340x365x20)	1	



- Check for Tensile Stress:

Max. Tensile force in each bracket = 20 tons
Tensile area = 4343 mm²

Permissible tensile stress = Yield strength x 0.6
= 250 MPa x 0.6
= 150 MPa

Tensile stress = Max. Tensile force / tensile area
= 200000/4343
= 46 MPa

The calculated tensile stress is less than permissible tensile stress value of 150 MPa and hence selected size and material of this part is safe for the tensile strength.

- Check for Shear Stress:

Max. Shear Force : 20 ton
Shear Area : 10361 mm²

Permissible shear stress is
= Yield Strength*0.4
= 250 MPa*0.4
= 100 MPa

Now, the shear stress is calculated as

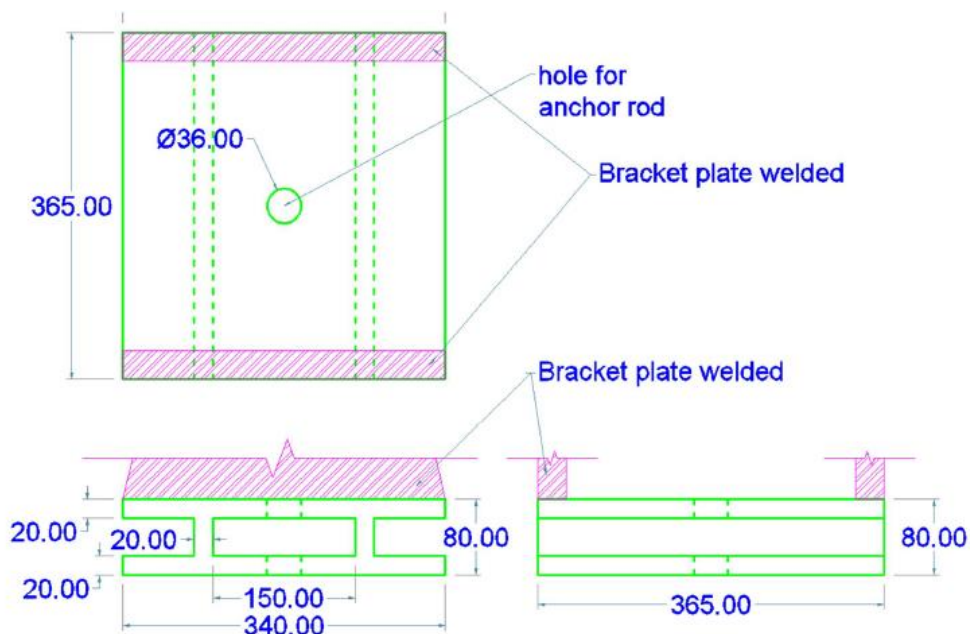
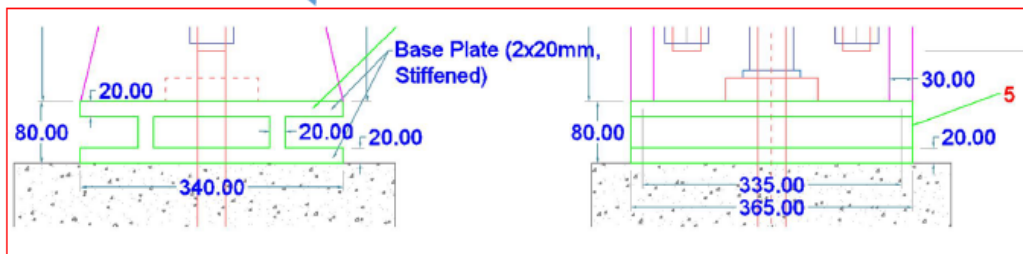
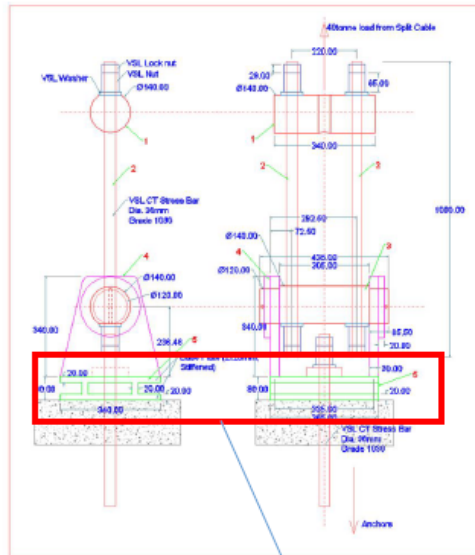
Max. Shear Stress = Max. Shear Force / Shear Area
= 20 ton/10361 mm²
= 19.30 MPa

Which is less than the permissible shear stress, hence the selected size and material of this part is safe for the shear strength.




8.1.4. Base-plate Connection

Cable-Anchor Connection						
Part List						
S.N.	Part Name	Material	Section	Dimensions (mm)	Qty.	Remarks
1	Adjustable Pin	Fe250	Round Bar	140 dia., L=340	1	
2	Thread Rod	VSL CT Stress Bar, Grade 1030	Thread rod	36 dia, L=1000	2	
3	Hinged Pin	Fe250	Round Bar	140 dia., L=340	1	
4	Bracket	Fe250	Plate 30	340x340x30	2	
5	Base Plate	Fe250	2x stiffened Plate 20	2x (340x365x20)	1	



- Check for Bending Stress:

3.0 <input checked="" type="checkbox"/> Calculation results					
3.1 Support number from left	R1	R2			
3.2 Reaction in supports	200198.59	200198.59			[N]
3.3 Bending moment Min. / Max.	Mo	0.00	33516.63		[Nm]
3.4 Beam deflection Min. / Max.	y	-0.116	0.000		[mm]
3.5 Bending stress Min. / Max.	σ_b	0	104.1		[MPa]
3.6 Weight of the beam	m		39.7		[kg]
3.7 Max. length of the free end (buckling).	Lmax		1630.3		[mm]
3.8 Relative beam deflection Max.	y'		0.035		[%]



Max. Bending Stress is calculated as 104 MPa, which is less than the permissible value i.e. 141 MPa. Hence the selected size of this part is safe for bending strength.

- Check for Shear Stress:

Max. Shear Force : 20 ton

Shear Area : 15200 mm²

Now, the shear stress is calculated as

Permissible shear stress is

$$= \text{Yield Strength} \times 0.4$$

$$= 250 \text{ MPa} \times 0.4$$

$$= 100 \text{ MPa}$$

$$\text{Max. Shear Stress} = \text{Max. Shear Force} / \text{Shear Area}$$

$$= 20 \text{ ton} / 15200 \text{ mm}^2$$

$$= 13.16 \text{ MPa}$$

Which is less than the permissible shear stress, hence the selected size and material of this part is safe for shear strength.



Signature

8.2. Ground Anchor Connection

The ground anchor design will check for numerous scenarios / failure modes, and different factors of safety are applied. The ground anchor design shall utilise different factors of safety for different failure mechanisms, minimum factors of safety are summarised below:

- Tendon capacity – 1.5
- Grout / Ground Interface – 3.0
- Grout / encapsulation interface 3.0
- Grout / tendon Interface 3.0

Anticipated Factored Loads are summarised below:

Factoring	Factored Lads for Various Cables (kN)		
	Main Cable (twin anchors)	Hand Cable	WindGuy Cable
Unfactored Load	260*	158	158*
Tendon capacity (factored) **	381*	237	237*
Grout / Ground Interface	762*	474	474*
Grout / encapsulation interface	762*	474	474*
Grout / tendon Interface	762*	474	474*
* Loads to be confirmed be Bridge Designer			
** Tendon Capacity also needs to be checked for potential corrosion / loss of capacity over design life			

The required fixed length to achieve the factored capacity on the ground/grout interface for the various cable anchors is summarised below:

Anchor Descriptions	'R' per Metre (kN)	Required Factored Capacity (kN)	Calculated Fixed Length (m)
Main Cable (two anchors per cable)	804.25	762	0.95
Hand Cable	804.25	474	0.59
WindGuy Cable	804.25	474	0.59

The calculated fixed anchor lengths are all less than the minimum recommended in BS8081, therefore a minimum 2m fixed length shall be adopted.



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9. CONCLUSION

1. As per received Design Summary & Compliance Report (Ref no. WE-RSG-SKYB-DSCR, Rev: 1.0) for Sky Bridge structure, below mentioned points has been noted.

- Maximum cable tension in main cable for each cable = 439.74 kN
- Maximum cable tension in each handrail cable = 157.44 kN

The Minimum Breaking Loads (MBL) for the selected cables are as follow;

- MBL for main cable – 48mm dia. 6x19 IWRC, 1960 N/mm² = 1614 kN
- MBL for handrail cable – 48mm dia. 6x19 IWRC, 1960 N/mm² = 1614 kN

With the above values, the factor of safety of the cables are resulted as;

- For main cable = 3.67
- For handrail cable = 10.25
- The total tension on main cable considering the load factors as per AISC LRFD-93, the factor of safety on main cable comes to be 2.46. However, safety factor of the main cable of 3.67 has been achieved. Hence both main cable & handrail cable are safe in tension.

2. As per received Design Summary Report of SAP Analysis of Deck Structure (Ref no. RN-WG-SKYB-DSDS, Rev: 0.0) for Sky Bridge structure.

- Maximum von mis stress (SVM) cross beam (ISMC 100) as 128.35 MPa noted from SAP 2000 analysis result which is within the permissible limit of maximum stress of 150 MPa.

3. As per received Design Summary & Compliance Report (Ref no. RN-WG-SKYB-DCCON, Rev: 0.0) for Sky Bridge structure, below mentioned points has been noted.

- All parts of Cable Anchor Connection are checked against the strength such as Bending, Shear & Tensile whichever is applicable and critical. The summary of strength check is shown below.

Sr. No	Part Name	Material	Section	Dimension (mm)	Qty.	Design Checks			
1	Adjustable Pin	Fe250	Round Bar	140 dia. L=340	1	Bending Strength	OK	Shear Strength	OK
2	Hinged Pin	Fe250	Round Bar	140 dia. L=340	1	Bending Strength	OK	Shear Strength	OK
3	Bracket	Fe250	Plate 30	340 x 340 x 30	2	Tensile Strength	OK	Shear Strength	OK
4	Base Plate	Fe250	2 x stiffener plate 20	2 x (340 x 365 x 20)	1	Bending Strength	OK	Shear Strength	OK

4. As per received Ground Anchor Design Philosophy Report (Ref no. 1799/TN01) for Sky Bridge structure, below mentioned points has been noted.

- The ground anchor design will check for different factor of safety are applied.
 - Tendon capacity = 1.5
 - Grout / Ground Interface = 3.0
 - Grout / encapsulation interface = 3.0
 - Grout / tendon Interface = 3.0

Anticipated Factored Loads are summarized below,

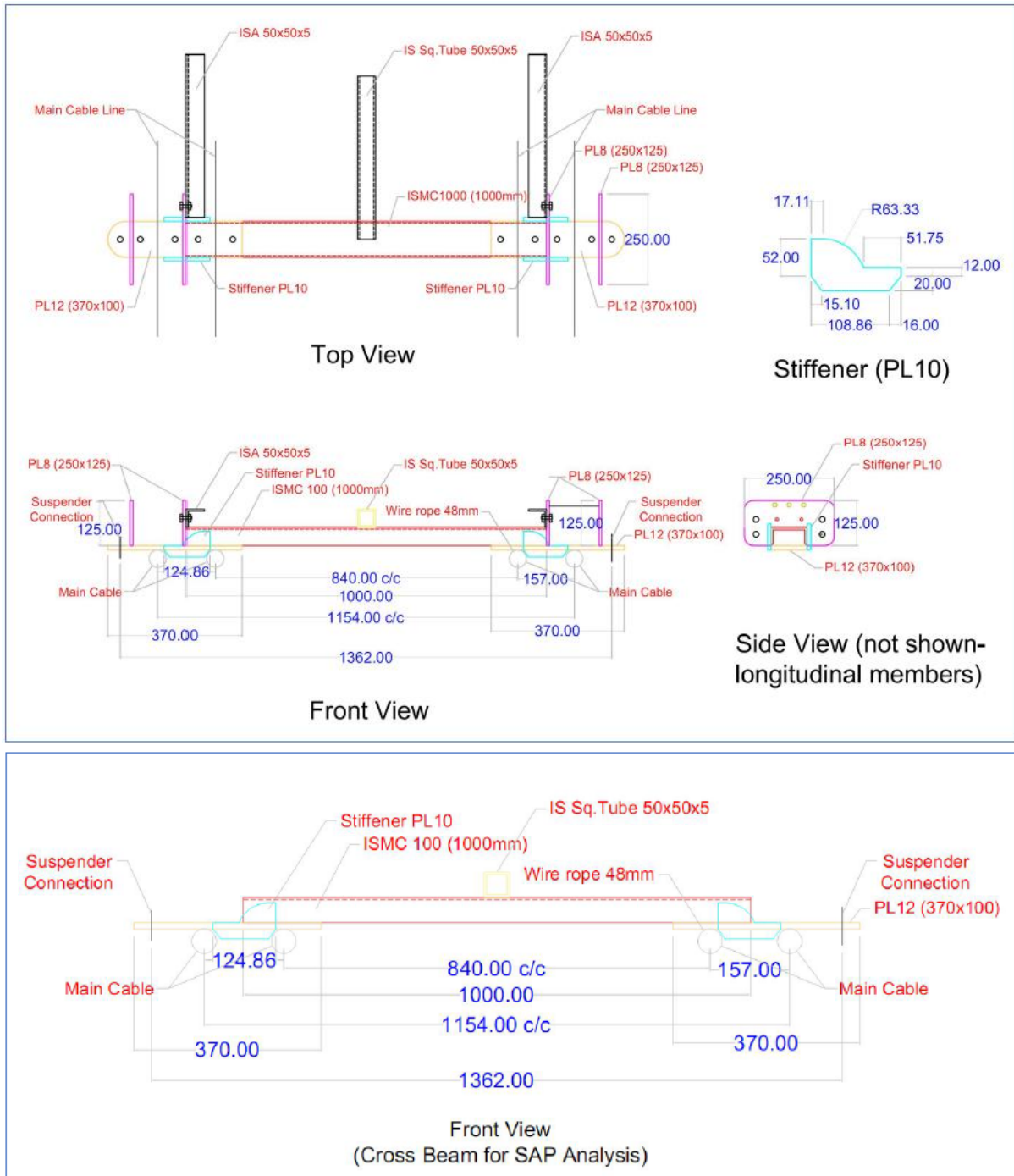
Factoring	Loads for Various Cables (kN)		
	Main Cable	Hand Cable	Windguy Cable
Unfactored Load	260	158	158
Tendon Capacity (Factored)	381	237	237
Grout/Ground Interface	762	474	474
Grout/Incapsulation Interface	762	474	474
Grout/Tendon Interface	762	474	474

- Detailed design will determine the required bar diameter. The proposed diameter high grade steel bar has a Yield Load of 960kN and Ultimate Load of 1070kN, which is significantly greater than the factored tendon strength requirement identified in the table above.
- The required fixed length to achieve the factored capacity on the ground/grout interface for the various cable anchors is 0.95m. However, the calculated fixed anchor lengths are all less than the minimum recommended in BS8081, therefore a minimum 2m fixed length shall be adopted. Hence it is safe for above stated load capacity.

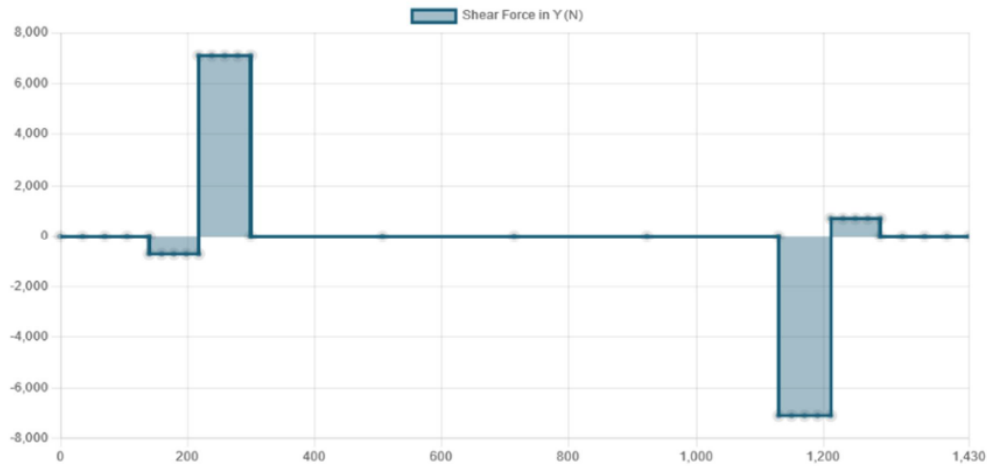
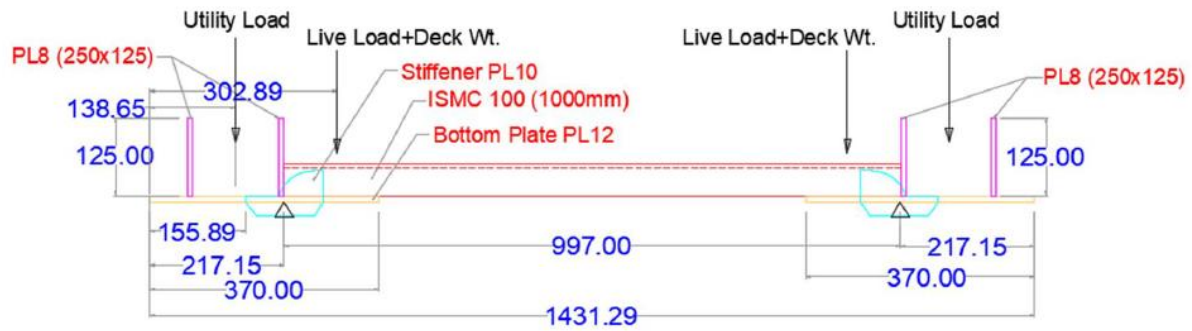


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5. As per received Design Calculations of End Connection of Cross Beam (Ref no. RN-WG-SKYB-DCECCB, Rev: 0.0) for Sky Bridge structure, below mentioned points has been noted.

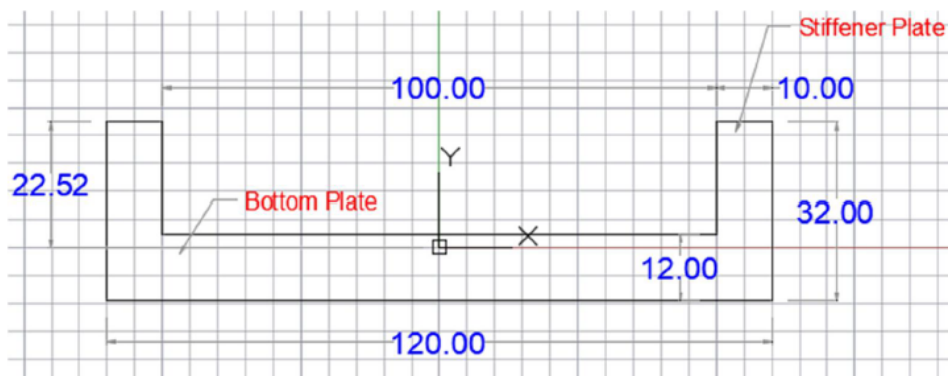


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Now, the bending moments and shear forces at each section-change positions are being calculated from the bending moment diagram (above), the values of which are

Location	Bending Moment	Shear Force
At stiffener location @ 218mm	56 Nm	7104 N
At end of the beam @ 156mm	13 Nm	720 N



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The section properties are

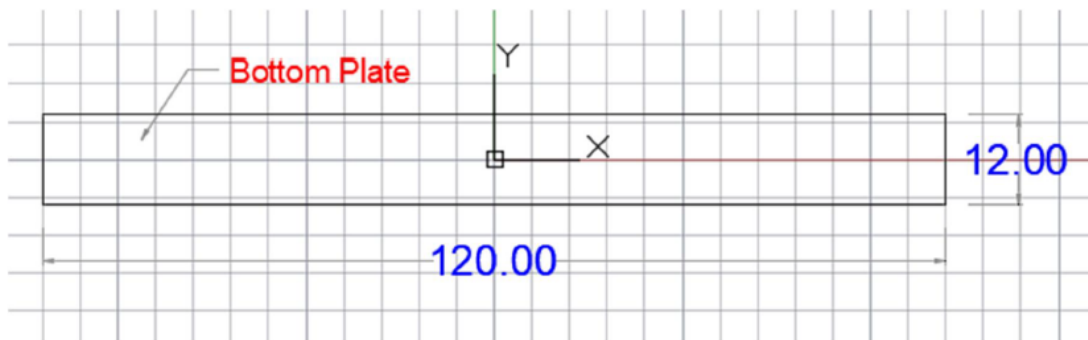
Cross Section Area	Area Moment of Inertia (X)	Section Modulus (X)
1840.00 mm ²	110752.469 mm ⁴	4917.96 mm ³

Bending stress is calculated a

$$\begin{aligned}\text{Bending Stress} &= \text{Bending Moment/Section Modulus} \\ &= 56 \text{ N-m}/4917.96 \text{ mm}^3 \\ &= 11.39 \text{ MPa} < 150 \text{ MPa, Hence} \quad \text{SAFE}\end{aligned}$$

$$\begin{aligned}\text{Shear Stress} &= \text{Shear Force/Cross Section Area} \\ &= 7104 \text{ N}/1840.00 \text{ mm}^2 \\ &= 3.86 \text{ MPa} < 140 \text{ MPa, Hence} \quad \text{SAFE}\end{aligned}$$

The cross section at the bottom plate location is



The section properties are

Cross Section Area	Area Moment of Inertia (X)	Section Modulus (X)
1440.00 mm ²	17280 mm ⁴	2880 mm ³

Bending stress is calculated a

$$\begin{aligned}\text{Bending Stress} &= \text{Bending Moment/Section Modulus} \\ &= 13 \text{ N-m}/2880 \text{ mm}^3 \\ &= 4.52 \text{ MPa} < 150 \text{ MPa, Hence} \quad \text{SAFE}\end{aligned}$$

$$\begin{aligned}\text{Shear Stress} &= \text{Shear Force/Cross Section Area} \\ &= 720 \text{ N}/1440.00 \text{ mm}^2 \\ &= 0.5 \text{ MPa} < 140 \text{ MPa, Hence} \quad \text{SAFE}\end{aligned}$$



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