Date: 01-08-2023

FOR PROPOSED DEVELOPMENT AT DRUMCOR, LOUGHDUFF, CO. CAVAN FOR KILLIAN BRADY & LISA MCDERMOTT

Submitted By



Miltron Glebe Carrigallen County Leitrim H12 PO25

✓ 086 208214616
✓ martin@mgdconsultants.ie

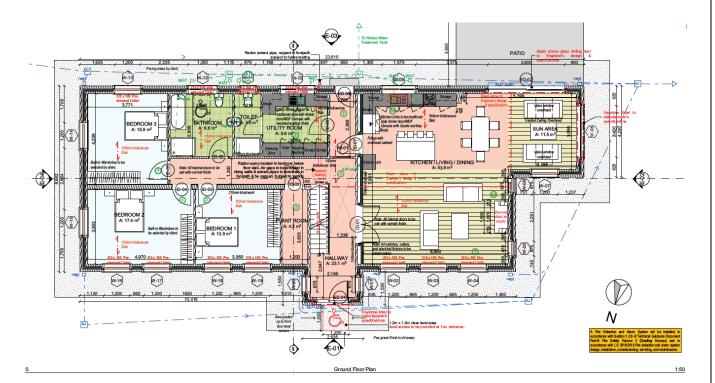
Revision: R1

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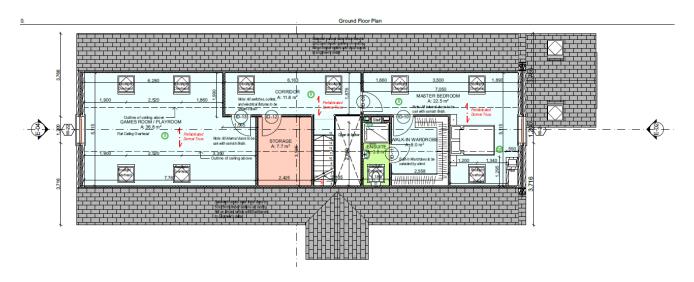
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1. INTRODUCTION

This document forms the Engineering Design Basis for Analysis and Design of Structural steel Members for proposed development at Drumcor, Loughduff, Co. Cavan.



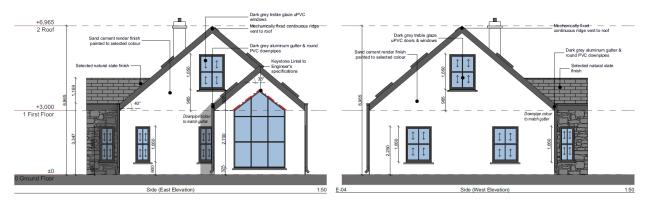
Proposed Ground Floor plan



Proposed First Floor plan



Proposed front and rear elevations



Proposed both side elevations

2. MATERIAL PROPERTIES

Material Specifications

Section Type	Hot rolled
Material grade	S355
Design Strength	355 N/mm ²
Density	78.33 kN/m ³
Modulus of elasticity "Es"	205.0kN/mm ²
Shear modulus "Gs"	78846.0 MPa
Poisson's ratio "μ"	0.3
Co-efficient of linear expansion	12*10 ⁻⁶ / °C

3. CODES CONSIDERED

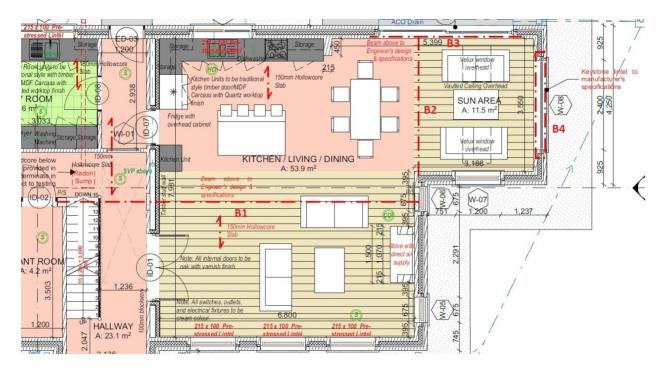
Following codes are referred for analysis and design of proposed structure.

- BS EN 1990 Eurocode Basis of Structural Design
- EN 1993-1-1 (2005) Eurocode 3: Design of steel structures Part 1-1: General rules and rules for buildings
- EN 1991-1-1 (2002) Eurocode 1: Actions on structures Part 1-1: General actions Densities, self-weight, imposed loads for buildings

4. **DESIGN ASSUMPTIONS**

• All members both end support conditions considered as pinned support, either supported on main steel member or on load bearing wall.

5. STRUCTURAL SYSTEM AND MEMBER LOCATION



Beam arrangement

6. LOADING DATA

6.1. Design Loads:

Building Design Loads will be in accordance with the more stringent of either the following criteria or as set forth by governing local and national codes. Structural design will be coordinated with architectural, mechanical and electrical drawings to ensure all loads impacting structural elements are adequately supported.

Load consideration/Assumptions:

Self-weight of 150mm Hollow core slab =	$3kN/m^2$
Weight considered for 75mm Screed (25kN/m2 x 0.075m)=	$1.875 kN/m^2$
Internal partition wall load on beam $= 0.5 \times 2.81 = 1.4$	1.4kN/m
(89mmtimber studs @ 600mm O.C. with 12.5mm plasterboard on	
both sides)	1 kN/m2
Internal partition wall load on slab per sq.m. slab area =	
External wall Build up =	4 kN/m^2
(12.5mm plasterboard + 100mm masonry + 40mm cavity + 110mm	
Xtratherm Cavitytherm+ 100mm masonry + 12.5mm plasterboard)	
Live load on floor (As per Category A of BS EN 1991-1-1:2002)=	$2kN/m^2$
Live load on stair (As per Category H of BS EN 1991-1-1:2002)=	$3kN/m^2$
Weight considered for Roofing material =	0.35 kN/m^2
Weight considered for Roof finishes =	0.2 kN/m^2

6.2. Load Combinations:

Design Load Combinations as per EN 1993-1-1 (2005) Eurocode 3:

• 1.35DL+1.50LL

Serviceability Load Combination as per EN 1993-1-1 (2005) Eurocode 3:

• DL+LL

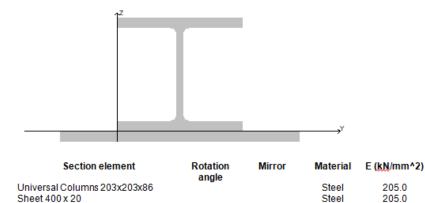
7. ANALYSIS AND DESIGN OF BEAM B1:

Analysis and design of steel Beam B1 performed in STAADPro software according to EN 1993-1-1 (2005) Eurocode 3:

Refer below image showing view of beam B1 modeled in STAADPro:



7.1. Member property:



The overall dimensions of the section are 400 x 242 mm

Basic geometry of the section							
	Parameter Cross sectional area	Value 19000.0	2				
Α		-0.0	mm ²				
α	rangio botti otti i E ana o v axoo		deg				
ſ*	Moment of inertia about axis parallel to Y passing through centroid	162689738.8	mm ⁴				
lz.	Moment of inertia about axis parallel to Z passing through centroid	137966668.53	4				
le le	Torsional moment of inertia (St. Venant)	2372246.41	mm ⁴				
Jac	Warping constant	0.0	mm ⁶				
Ĩ¥	Radius of gyration about axis parallel to Y passing through centroid	92 . 53	mm				
ĺε	Radius of gyration about axis parallel to Z passing through centroid	85 . 21	mm				
Wut	Elastic modulus about U-axis (+ye extreme)	1003703.33	mm ³				
Wu	Elastic modulus about U-axis (-ye extreme)	2030816.07	mm ³				
W _{k+}	Elastic modulus about V-axis (+ye extreme)	689833.34	mm ³				
W	Elastic modulus about V-axis (-ye extreme)	689833.34	mm ³				
Walu	Plastic modulus about axis parallel to U-axis	1287316.7	mm^3				
Walx	Plastic modulus about axis parallel to V-axis	1255891.51	mm^3				
Ju .	Moment of inertia about U-axis	162689738.8	mm ⁴				
Ϊν	Moment of inertia about V-axis	137966668.53	4				
برأ	Radius of gyration about U-axis	92.53	mm				
Ϊν	Radius of gyration about V-axis	85.21	mm				
a _{u+}	Centroid to edge of compression zone along +ye U-axis	36 . 31	mm				
a _u .	Centroid to edge of compression zone along -ve U-axis	36 . 31	mm				
a ×+	Centroid to edge of compression zone along +ve V-axis	52.83	mm				
a _w	Centroid to edge of compression zone along -ve V-axis	106.89	mm				

7.2. Load calculation of beam B1

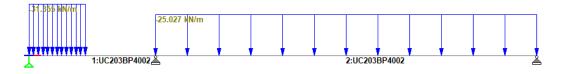
Calculation of Dead and Live load on STEEL Beam:

Span of loading as shown in above Figure 7 and Figure 8,

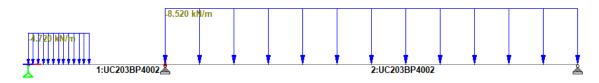
Loading between node 1-2

Dead Load

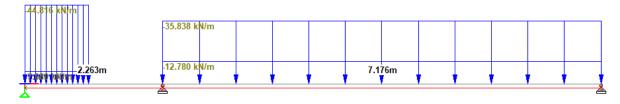
S.W of steel beam		Program Calcula per sect properti	ited as
Load due to Laminate floor= (1.875 kN/m ² x 2.36m tributar	ry span)=	4.425	kN/m
Self-weight of hollow core slab = (3 x2.36 m tributary spar Uniformly distributed load of staircase (self weight+step wt+ floor finish + live load) x span/2	n)=	7.08	kN/m
$(25x0.15x[305/230] + 25x0.5x0.2+1+3) \times 3.245/2 =$ Internal partition wall load on beam		18.49	kN/m
$(1.00 \text{kN/m}^2 \text{x} \ 2.36 \text{ m tributary span}) =$		2.36	kN/m
	Total Dead load on beam=	31.33	kN/m
Live load			
Live load on floor = $(2 \text{ kN/m}^2 \text{x} (4.72 \text{ m/2}))$ =		4.72	kN/m
	Total live load on beam=	4.72	kN/m
Loading between node 3-4			
Dead Load			
S.W of steel beam		Program Calcula per sect	ited as
Load due to Laminate floor= (1.875 kN/m ² x 4.26m tributar	w cnan)—	7.987	kN/m
Self weight of hollow core slab = $(3 \text{ kN/m}^2 \text{x} 4.26 \text{ m tributar})$		12.78	kN/m
Internal partition wall load (1.00kN/m ² x 4.26m tributary space)	•	4.26	kN/m
	Total Dead load on beam=	25.02	kN/m
Live load			
Live load on floor = $(2 \text{ kN/m}^2 \text{x } 4.26 \text{ m tributary span})$ =		8.52	kN/m
Total Live load on beam		8.52	kN/m
Total Live load on beam		0.52	K1 4/ 111



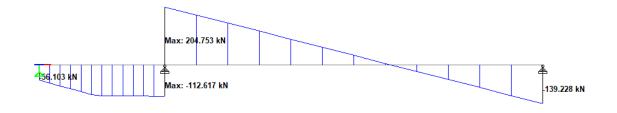
Dead load on beam B1



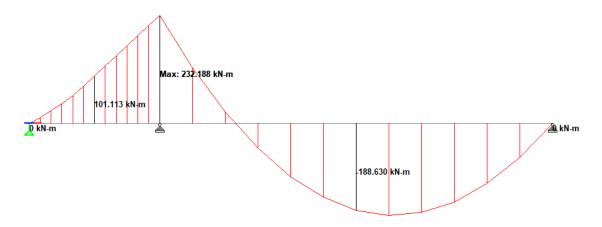
Live load on beam B1



Loading Diagram (1.35DL+1.5LL)



Shear force diagram (1.35DL+1.5LL)



Bending Moment Diagram (1.35DL+1.5LL)

7.3. Utilization ratio check

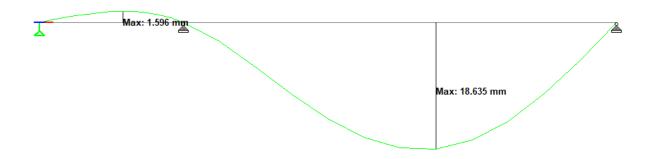


Utility ratio of Beam B1

Above Figure shows member utilization ratio. Failed members (i.e., members having utility ratio more than 1) will be highlighted with red colors. It can be seen from image that all members are green. Hence, all members have passed in design.

7.4. Deflection check

Below image shows displacement diagram of member having maximum vertical deflection for serviceability load combinations.



Deflection diagram of beam B1 (DL+LL)

Maximum vertical displacement of beam in Y direction= 18.635 mm

Permissible vertical deflection = Span / 360 = 7176 / 360 = 19.93 mm

Actual maximum vertical deflection of beam = 18.635 mm < 19.93 mm (Hence, OK)

7.5. STAAD design output results

STAAD output results for BEAM B1 Member 1 (2.26m):

```
2.263m
                                         7.176m
                                         2:UC203BP4002
       _____
           1 ST UC203BP4002 (UPT)
                                              0.083
                      PASS EC-6.2.5
                       0.00
                                  0.00
                                            -232.19
       _____
        MATERIAL DATA
          Grade of steel
                            = S 355
          Modulus of elasticity = 205 kN/mm2
          Design Strength (py) = 355 N/mm2
        SECTION PROPERTIES (units - cm)
          Member Length = 235.20
          Gross Area = 190.00
                            Net Area = 190.00
                                  z-axis
                                         13800.001
          Moment of inertia : 16300.001
Plastic modulus : 7879.602
                                            10714.416
          Elastic modulus
                            : 1346.551
                                             690.173
                                 0.000
          Shear Area
                            :
                                               0.000
          Radius of gyration :
                                  9.262
                                               8.522
          Effective Length
                            : 235.200
                                              235.200
        DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005
          Section Class : CLASS 1
          Squash Load
          Axial force/Squash load :
                                 0.000
                     GM1 : 1.00
          GM0 : 1.00
                                          GM2 : 1.25
                                             y-axis
                                  z-axis
          Slenderness ratio (KL/r) :
                                    25.4
                                 4496.2
          Compression Capacity :
          Tension Capacity :
                                 6703.2
                                              3803.6
          Moment Capacity
                            : 2797.3
                                             3803.6
          Reduced Moment Capacity : 2797.3
          Shear Capacity
                                    0.0
        BUCKLING CALCULATIONS (units - kN,m)
          Lateral Torsional Buckling Moment MB = 2797.3
          co-efficients C1 & K : C1 =1.000 K =1.0, Effective Length= 2.352
          Lateral Torsional Buckling Curve :
          Compression buckling curves: z-z:
         Critical Load For Torsional Buckling, NcrT = 56638.6
                                              у-у:
         STAAD SPACE
                                                     -- PAGE NO.
        CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):
        CLAUSE RATIO LOAD FX VY VZ
                                                  MZ
                   0.083 3 0.0 112.6 0.0 -232.2
                                                       0.0
        EC-6.2.5
                              0.0 112.6
                                           0.0 -232.2
        EC-6.3.2 LTB 0.083 3
```

STAAD output results for BEAM B1 Member 2 (7.176m):

1:UC203BP4002

2.263m

		. ,			
MEMBER TAI	LE RESULT				
	FX		MY		LOCATIO
			========		
2 ST 1	IC203BP4002 (UPT	(1)			
	PAS	•	EC-6.2.5	0.083	3
	0.00		0.00	232.19	0.00
MATERIAL DAT	'A				
Grade of	steel	=	S 355		
	of elasticity				
Design St	rength (py)	=	355 N/mm2		
	ERTIES (units -				
	ngth = 708.7 a = 190.00		Net Area -	190 00	
STAAD SPAC			Net Area =	190.00	PAGE NO
JIANU JIAN					PAGE N
			z-axis		
Moment of	inertia	:	16300.001	13800.001	l
Plastic r	odulus	:	7879.602	10714.416	5
Elastic r	odulus	:			
Shear Are		:	0.000	0.000	9
Radius of	gyration Length	:	9.262	8.522	
Effective	Length	:	708.700	708.700	9
DESTEN DATA	(mathe later)		20000 110 2 /	/2225	
Section ((units - kN,m)			2005	
Squash Lo	.1055 .he	:	CLASS 1 6745.00		
	ce/Squash load				
GM0 : 1.				GM2 : 1.25	
0.0 . 2.	-		2100	0.12 1 2123	
			z-axis	y-axis	
Slenderne	ss ratio (KL/r)	:			
Compressi	on Capacity	:	1469.6	1332.9	
Tension (:			
		:			
	loment Capacity				
Shear Cap	acity	:	0.0	0.0	
BUCKLING C	ALCULATIONS (unit	ts - I	kN,m)		
	Torsional Buckl:				
	cients C1 & K : (ffective Length	1= 7.087
	Torsional Buckli				
compres	sion buckling cu l Load For Torsio	rves:	z-Z: Ruckling	y-y: NcrT = 19	005 0
	DADS FOR EACH CLA				1033.3
CL AUSE	RATTO LOAD		FY VV	V7 M7	MY
EC-6.2.5	0.083 3 TB 0.083 3		0.0 204.8	0.0 232.2	0.0
EC-6.3.2 L	TB 0.083 3		0.0 204.8	0.0 232.2	0.0
STAAD SP	ACE				- PAGE NO.

Torsion has not been considered in the design.

7.176m

8. ANALYSIS AND DESIGN OF BEAM B2:

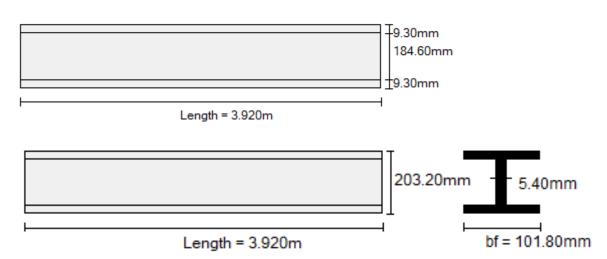
Refer below image showing view of beam B2 modeled in STAADPro:



Beam B2 Dimensions

8.1. Member Property

Beam no. = 1. Section: UB203X102X23



8.2. Load calculation of beam B2

Calculation of Dead and Live load on Beam B2:

Span of loading as shown in above Figure,

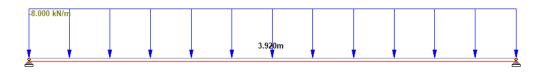
Dead Load

S.W of steel beam

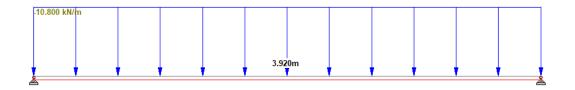
Program Calculated as per section property

External wall build up wall load on beam (4kN/m² x 2m triangle tributary height)=

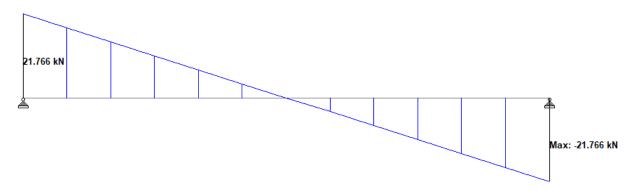
8 kN/m



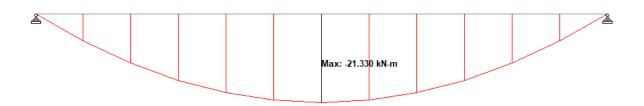
Dead load on beam B2



Loading Diagram (1.35DL+1.5LL)



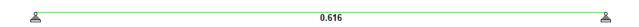
Shear force diagram (1.35DL+1.5LL)



Bending Moment Diagram (1.35DL+1.5LL)

..

8.3. Utilization ratio check



Utilization ratio of Beam B2

Above Figure 12 shows member utilization ratio. Failed members (i.e., members having utility ratio more than 1) will be highlighted with red colors. It can be seen from image that all members are green. Hence, all members have passed in design.

8.4. Deflection check

Below figure shows displacement diagram of member having maximum vertical deflection for serviceability load combinations.



Deflection diagram of beam B2 (DL+LL)

Maximum vertical displacement of beam in Y direction= 5.842 mm

Permissible vertical deflection = Span / 360 = 3920/360 = 10.888 mm

Actual maximum vertical deflection of beam = 5.842 mm < 10.88 mm (Hence, OK)

8.5. STAAD design output results

STAAD output results for BEAM B2 Member 1:

			UB203X102)	(23		
MEMBER	TABLE	RESULT/ FX	CRITICAL CON	ID/ RATIO/	LOADING/ LOCATION	
=======						
1 ST	UB203X10	0X23 (BRITI	SH SECTIONS)			
		•		TB 0.616	3	
		0.00	0.00	-21.33	1.96	
MATERIAL						
	of steel					
		_	205 kN/mm2			
Design	n Strength	(py) =	: 355 N/mm2			
SECTION I	DDODEDTIES	/units /				
	PROPERTIES r Length =					
	_		Net Area =	29 40		
Gross	Ared = A	29.40	Net Area =	29.40		
			z-axis	y-axis		
Moment	t of inert	ia '	2100.000			
	ic modulus		234.000			
	ic modulus					
	Area			32.220		
			17.041	12.381		
rauiu:	s or gyrac.	LOII	8.452 392.000	2.362 392.000		
ETTEC	tive tengti	'	392.000	392.000		
DESTAN D	ATA /unite	LN m	EUROCODE NO.3	/2005		
DESIGN DA	on Class	- KNJIII)	CLASS 1	/ 2005		
Sausel	b Load		1043.70			
			0.000			
			1.00	GM2 + 1 25		
ane .	1.00	GMI .	1.00	GHZ : 1.25		
			z-axis			
	erness rati					
Compre	ession Capa	ecity :	926.1	188.5		
			1037.2			
	t Capacity					
	ed Moment (
Shear	Capacity	:	349.3	253.8		
BUCKLING CAL	CIII ATTONS	(units - k	N m)			
			ment MB	- 34.6		
				fective Length=	2 920	
			rve : CURVE b	rective teligin=	3.520	
	ritical Mo	_		Mcr =	35.7	
			•			
			uckling,	e a y-y: Cur		
				NcrT = 98 ng, NcrTF = 98		
Cilcicul	LOUG FOI I	013101101-1	icxurui buckii	ing, NCI II - 3	52.5	
STAAD SPAC	E				PAGE NO. 4	
	DS FOR EAC	H CLAUSE C	HECK (units- k	N,m):		
CRITTCAL LOAD			(with the K			
	RATTO	LOAD F	X VV	V7 M7	MY	
CLAUSE		LOAD F		VZ MZ	MY a a	
CLAUSE EC-6.2.5	0.257	3 0	.0 0.0	0.0 -21.3	0.0	
CLAUSE	0.257 0.086	3 0 3 0		0.0 -21.3 0.0 0.0	0.0 0.0	

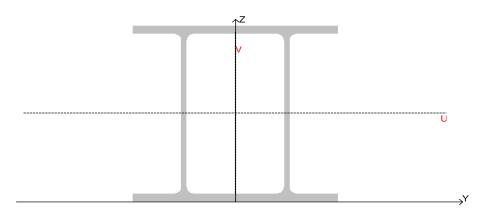
9. ANALYSIS AND DESIGN OF BEAM B3:

Refer below image showing view of beam B3 modeled in STAADPro:



Beam B3 Dimensions

9.1. Member Property



Section element	Rotation angle	Mirror	Material	E (kN/mm^2)
Universal Beams 203x102x23			Steel	205.0
Universal Beams 203x102x23			Steel	205.0

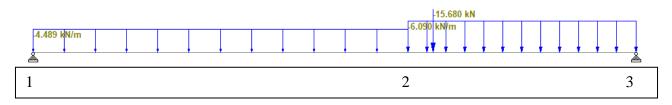
The overall dimensions of the section are 204 x 203 mm

Basic geometry of the section

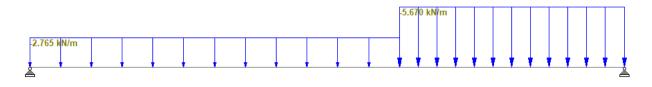
	Parameter	Value	
A	Cross sectional area	5879.8	mm^2
a	Angle between Y-Z and U-V axes	-0.0	deg
I_y	Moment of inertia about axis parallel to Y through centroid	passing42097868.57	mm ⁴
I_z	Moment of inertia about axis parallel to Z through centroid	passing 18510848.38	mm ⁴
I_t	Torsional moment of inertia (St. Venant)	140388.92	mm^4
\mathbf{i}_{y}	Radius of gyration about axis parallel to Y through centroid	passing84.62	mm
i_z	Radius of gyration about axis parallel to Z through centroid	passing 56.11	mm
W_{u+}	Elastic modulus about U-axis (+ve extreme)	414349.11	mm^3
W_{u-}	Elastic modulus about U-axis (-ve extreme)	414349.11	mm^3
W_{v+}	Elastic modulus about V-axis (+ve extreme)	181835.44	mm^3
W_{v-}	Elastic modulus about V-axis (-ve extreme)	181835.44	mm^3

9.2. Load calculation of beam B3

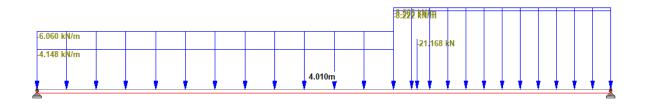
Calculation of Dead and Live load on Beam:		
Span of loading as shown in above image,		
Self-weightconsidered for 150mm Hollow core slab =	3	kN/m^2
Weight considered for Laminate flooring (25kN/m2 x 0.075m)=	1.875	kN/m^2
Live load on floor (As per Category A of BS EN 1991-1-1:2002)=	2	kN/m^2
Live load on roof (As per Category H of BS EN 1991-1-1:2002)=	1	kN/m^3
Weight considered for 350mm external wall build up =	4	kN/m^2
Weight considered roofing material =	0.35	kN/m^2
Weight considered for roof finishes =	0.2	kN/m^2
Loading between node 1-2		
Dead Load		
S.W of steel beam External well heild on light heart (4 hN/m ² v 0.742m tributom)	Prograi	n Calculated
External wall build-up load on lintel beam(4 kN/m ² x 0.742m tributary height)=	2.968	kN/m
Roofing material load on beam(0.35 kN/m ² x 2.765 m tributary roof		
span)=	0.9677	kN/m
Roof finishes load on beam $(0.2 \text{ kN/m}^2\text{x } 2.765\text{m tributary roof span})=$	0.553	kN/m
Total Dead load on beam=	4.4887	kN/m
Live load	2.55	137/
Live load on Roof = $(1 \text{ kN/m}^2 \text{x } 2.765 \text{m tributary roof span})$ =	2.765	kN/m
Total live load on beam=	2.765	kN/m
Loading between node 2-3		
Dead Load	D	1-4-1
S.W of steel beam	Program Calcusection	nated as per
External wall buildup load on lintel beam(4 kN/m² x 0.742m tributary		
height)=	2.968	kN/m
Roofing material load on beam $(0.35 \text{ kN/m}^2\text{x} 5.67 \text{ m tributary roof span})=$	1.9845	kN/m
Roof finishes load on beam $(0.2 \text{ kN/m}^2\text{x} 5.67\text{m} \text{ tributary roof span})=$	1.134	kN/m
Total Dead load on beam=	6.0865	kN/m
Live load		
Live load on Roof = $(1 \text{ kN/m}^2 \text{x } 2.765 \text{m tributary roof span})$ =	5.67	kN/m
Total live load on beam=	5.67	kN/m
Load from secondary beam Concentrated load from Beam B2 on Beam B3=	15 60	1 ₂ NJ
Concentrated toad from Beam B2 on Beam B3=	15.68	kN



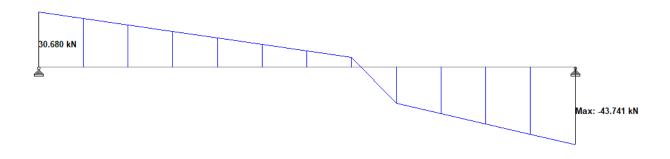
Dead load on beam B3



Live load on beam B3



 $Loading\ Diagram\ (1.35DL+1.5LL)$

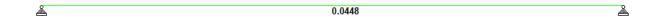


Shear force diagram (1.35DL+1.5LL)



Bending Moment Diagram (1.35DL+1.5LL)

9.3. Utilization ratio check

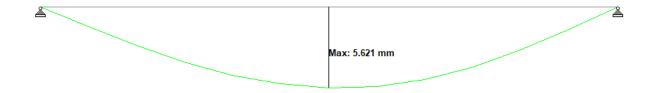


Utilization ratio of Beam B2

Above shows that failed members (i.e., members having utility ratio more than 1) will be highlighted with red colors. It can be seen from image that all members are green. Hence, all members have passed in design.

9.4. Deflection check

Below image shows displacement diagram of member having maximum vertical deflection for serviceability load combinations.



Deflection diagram of beam B2 (DL+LL)

Maximum vertical displacement of beam in Y direction= 5.621 mm

Permissible vertical deflection = Span / 360 = 4010/360 = 11.138 mm

Actual maximum vertical deflection of beam = 5.621 mm <11.138 mm (Hence, OK)

9.5. STAAD design output results

STAAD output results for BEAM B3 Member 1:

```
MEMBER TABLE
                  RESULT/ CRITICAL COND/ RATIO/ LOADING/
                    FX MY MZ
                                                       LOCATION
_____
     1 ST 4UB203 (UPT)
                   PASS EC-6.2.5
0.00 0.00
                                                0.045
                                             -42.98
 MATERIAL DATA
    Grade of steel
                          = S 355
    Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 355 N/mm2
 SECTION PROPERTIES (units - cm)
    Member Length = 401.00
    Gross Area = 58.80
                              Net Area = 58.80
                                 z-axis
                     : 4209.791
: 2703.191
                        : 4209.791
                                             1851.080
    Moment of inertia
    Plastic modulus
    Elastic modulus
                         : 414.758
                               0.000
    Shear Area
                         :
                                               0.000
    Radius of gyration : 8.462
Effective Length : 401.000
                                 8.462
                                                5.611
                                              401.000
 DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005
                   : CLASS 1
    Section Class
    Squash Load
                         : 2087.33
    Axial force/Squash load : 0.000
    GM0 : 1.00
                GM1 : 1.00
                                         GM2 : 1.25
                                              y-axis
                               z-axis
    Slenderness ratio (KL/r) :
                                  47.4
    Slenderness ratio (KL/r): 47.4
Compression Capacity: 769.1
Tension Capacity: 2074.4
Moment Capacity: 959.6
                                              2074.4
                                959.6
                                               832.7
    Reduced Moment Capacity : 959.6
    Shear Capacity
   BUCKLING CALCULATIONS (units - kN,m)
     Lateral Torsional Buckling Moment
                                      MB = 959.6
     co-efficients C1 & K : C1 =1.000 K =1.0, Effective Length= 4.010
     Lateral Torsional Buckling Curve :
    Compression buckling curves: z-z: y-y:
Critical Load For Torsional Buckling, NcrT = 3401.7
    STAAD SPACE
   CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):
   CLAUSE RATIO LOAD FX VY VZ
                                                  MZ
                                                         MY
  EC-6.2.5 0.045 3 0.0
EC-6.3.2 LTB 0.045 3 0.0
                                 -20.6 0.0 -43.0
-20.6 0.0 -43.0
   Torsion has not been considered in the design.
```

10. ANALYSIS AND SPECIFICATION OF Lintel beam B4:

10.1. Load calculation of Lintel beam B4

Dead Load

S.W of lintel beam External wall build up wall load on lintel beam(4 kN/m²x0.62m tributary height) =

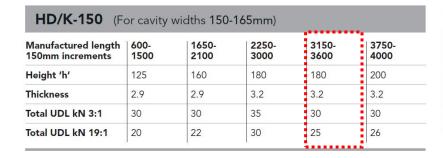
2.48 kN/m

Span of lintel beam B4 = 3.2 m

Total UDL load on $B4 = 2.48kN/m \times 3.2m = 8 kN$

10.2. Lintel specification from manfacturer

Keystone lintel: HD/K-150 for length 3150-3600



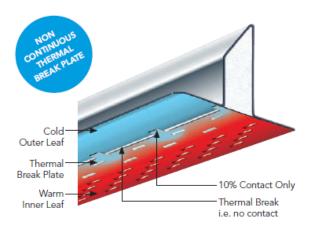


Keystone lintel illustration & specification

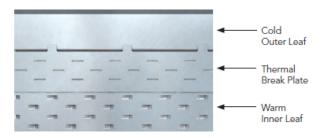
Actual capacity of lintel HD/K-150 = 25kN > 8kN (Actual Loading)

STANDARD KEYSTONE LINTEL

with patented Thermal Break Plate



Standard Keystone Lintel with patented non continuous Thermal Break Plate



GALVANISED STEEL

Keystone's standard range of lintels are manufactured from high quality grade pre-galvanised mild steel to BS EN 10346:2009 DX51D plus Z600 or grade Z275 to BS EN10025-2:2004 with minimised spangle finish and a minimum yield stress of 250N/mm².

STAINLESS STEEL

Please refer to page 53 for details.

STRUCTURAL PERFORMANCE

The Keystone Lintel range has safe working loads as detailed in each applicable loading table in our Lintel Range and Loading tables, pages 11-53. The structural performance figures within each table have been ascertained by testing in accordance with the requirements of standards BS 5977 Part 2: 1983 and BS EN 845-2:2003.

The figures take into account the different loading arrangements which are common to traditional cavity wall construction.

Differential Total UDL kN 3:1 Up to 75% loading on the inner leaf.

Differential Total UDL kN 19:1 Up to 95% loading on the inner leaf.

LINTEL LOAD TABLES

For full details of load tables specific to your lintel type please see Lintel Range & Loading Tables pages 11-53.

Differential Load 3:1 ratio, 75% load on inner leaf. Differential Load 19:1 ratio, 95% load on inner leaf.

Lintel types: HD/K, S/K-50 (215WIL), S/K-70 (215WIL), S/K-90 (215WIL), S/K-110, S/K-130, S/K-150, SB/K, T/K, SL/K, RB/K, TJ/K, TW/K, INT/K, SW/K, IB/K, EL/K-50, EL/K-90, CFS/K, X/K have been tested as a composite unit with surrounding masonry, built in accordance with BS EN 1996-2:2006. These composite units have been tested in accordance with the requirements of BS5977: part 2: 1983 (BS EN 845-2:2003).